

## **DETERMINATION OF ABSORPTION COEFFICIENT OF FIBRE GLASS/EPOXI RESIN COMPOSITE MATERIALS THROUGH ULTRASONIC TECHNIQUES**

**MARIANA DOMNICA STANCIU, IOAN CURTU<sup>1</sup>**

**Abstract.** Nowadays, the composite have numerous applications in different sectors. For these reasons, it's important to know the physical, mechanical/dynamical and acoustical properties of composites materials and in accordance with needs to improve some of properties. The paper presents the experimental results regarding sound absorption coefficient of fibre glass /epoxi resin composites, using ultrasound method based on elastic wave absorption in solid medium. The rectangular plane plates classified in 4 types in accordance with composites structures were tested. The tests revealed the anisotropic properties of composites and the capacity of plates to attenuate the high frequencies. The acoustic attenuation coefficient is influenced by thickness of plates and the pressure used to obtain the composite.

**Keywords:** woven composite, ultrasound, sound absorption coefficient, anisotropy

### **1. INTRODUCTION**

One of the highlights of these technological advances is the ultrasound evaluation technique, an important tool with the potential to improve this material's quality and competitiveness [1].

The use of ultrasonic wave propagation as a nondestructive evaluation technique has proved to be a viable method to characterize wood. Research on ultrasound techniques has evidenced the efficacy of the method to determine the mechanical properties of wood (Bucur, 1984). Ultrasonic methods (NDT) in examining composite materials allows the highlighting of materials discontinuities and the determination of important properties such as elastically modulus, Poisson coefficient, hardness, acoustic attenuation coefficient and to obtain qualitative information about internal structure and porosity of the tested samples. The literature review presents numerous studies on determination of mechanical, thermal and acoustic properties through different methods [1,2,8]. This paper focuses on determination of sound

---

<sup>1</sup> *Transilvania University of Brasov, Romania, mariana.stanciu@unitbv.ro, curtui@unitbv.ro*

absorption coefficient of composite made from fiberglass and epoxy resin using the method of absorbing elastic waves (ultrasound) in solid medium [3, 6, 7].

## 2. MATERIALS AND METHOD OF INVESTIGATION

The investigation method is based on determine absorption of elastic waves in solid medium [4,9]. Wave absorption represents the direct conversion of ultrasound wave energy in heat. The absorbed energy increases with increasing of ultrasonic wave frequencies. Due to attenuation, ultrasound pressure decreases with increasing the distance from sound source. If the change of pressure is noted with  $dP$  covering a distance  $dx$ , then:

$$dP = -\alpha P dx \quad (1)$$

the minus indicate the decreasing of sound pressure,  $\alpha$  – attenuation constant.

Integrating relation (1) is obtained:

$$\int_{P_0}^P \frac{dP}{P} = -\alpha \int_{x_0}^x dx \quad \text{or} \quad \ln \frac{P}{P_0} = -\alpha(x - x_0). \quad (2)$$

Noting with  $d=x-x_0$ , the distance of wave propagation, is obtained:

$$P = P_0 e^{-\alpha d} \quad (3)$$

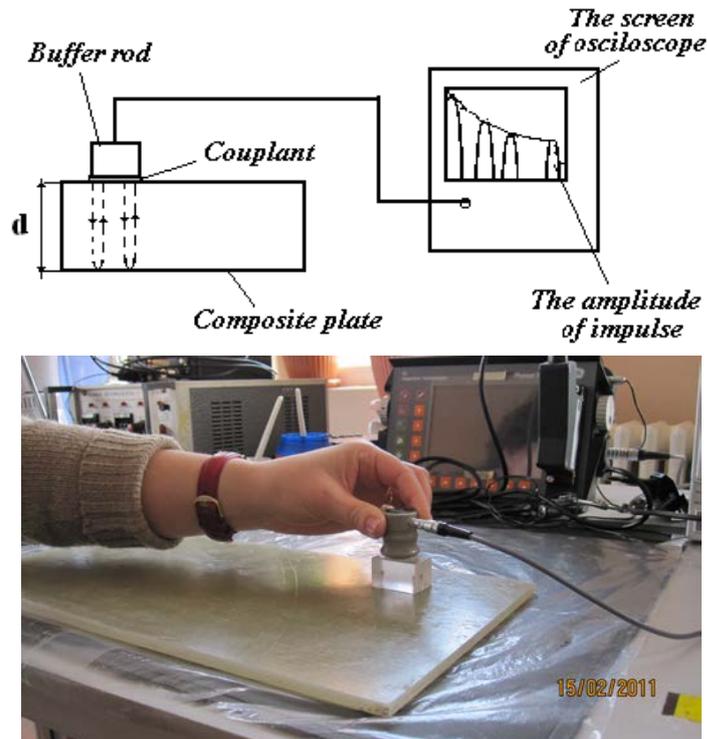
The measurements of ultrasound pressure in two points separated by distance  $d$  allows the determination of values  $P_1$  and  $P_2$ . Attenuation coefficient is measured in dB/m and is determinates with the relation:

$$\alpha = \frac{20 \log \frac{P_1}{P_2}}{d} [\text{dB} / \text{m}] \quad (4)$$

Depending on the values of attenuation coefficient, the materials are classified into:

- a) materials with  $\alpha$  low attenuation coefficient  $<10$  [dB / m].
- b) materials with attenuation coefficient range between 10 [dB/m] and 100 [dB/m]. For materials such as
- c) materials with high values of attenuation coefficient over 100 [dB / m].

The experimental equipment consisted of a control ultrasound, oscilloscope, buffer rod for longitudinal and transversal waves, samples made from various materials, means of measurement of distance. The experimental set-up is shown in Figure 1.



**Fig.1.** Experimental Set-up

The attenuation coefficient and ultrasound speeds were determined using pulse-echo method. The control equipment (Fig.1) which connects the buffer rod contains a cathode ray tube whose screen is observed, the applied voltage pulse encoded and successive wave reflections on opposite sides of the parts tested. The experimental investigations were conducted in non-destructive testing laboratory of the National Institute for technical Physics of Iasi, coordinated by Prof. Dr. Raimond Grimberg.

The studied samples were rectangular plates made from fibre glass/epoxy resin composite with different structures (number of stratimat layers and fiberglass layers). For each structure, were carried out 15 samples and nondestructive test on acoustic attenuation properties wre performed on plates with good quality of surfaces. The buffer rod with longitudinal wave with frequency 4 MHz was coupled at the control device and was applied on the plate by means of ultrasonic coupling. Before tests, the weight and thickness of plates were determined (Table 2 and Figure 2).

Table 1. The structure of composite plates

Categories of plates	Resin	Structure	Sizes Lxlxh	Type of pressure
Composite 1 (15 samples)	unsaturated polyester resin based on dicyclopentadiene and orthophthalic acid dissolved in styrene.	4 layers of stratimat (300 g/m <sup>2</sup> ) 3 layers of fibreglass	400x200x4	Normal pressure
Composite 2 (15 Samples)		5 layers of stratimat (300 g/m <sup>2</sup> ) 4 layers of fibreglass	400x200x6	Normal pressure
Composite 3 (15 Samples)		6 layers of stratimat (300 g/m <sup>2</sup> ) 4 layers of fibreglass	400x200x6	Low pressure
Composite 4 (15 Samples)		6 layers of stratimat (300 g/m <sup>2</sup> ) 4 layers of fibreglass	400x200x5	High pressure

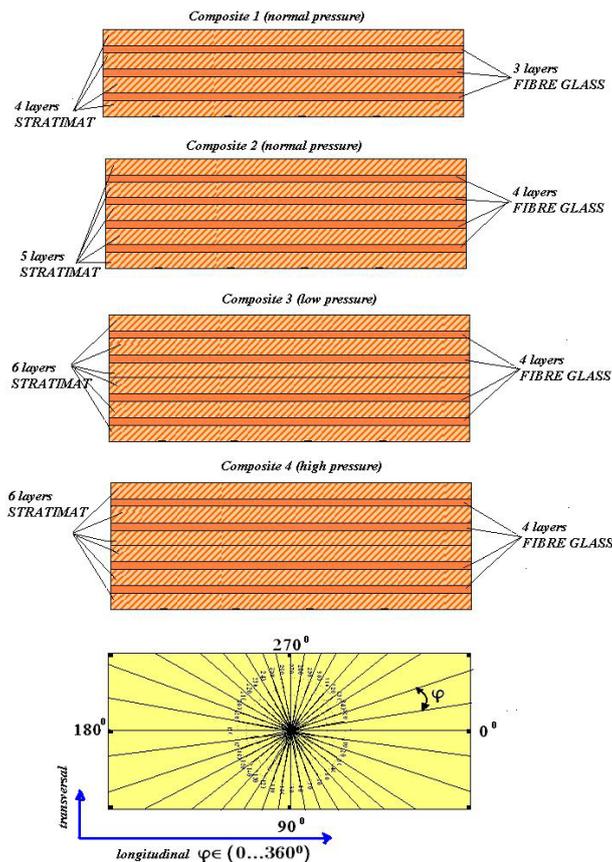


Fig.2. The structure of composite materials

Table 2. The characteristics of samples

Code	Composite 1		Code	Composite 2		Code	Composite 3		Code	Composite 4	
	Weight w [kg]	Thickness d [mm]		Weight w [kg]	Thickness d [mm]		Weight w [kg]	Thickness d [mm]		Weight w [kg]	Thickness d [mm]
16	0.520	4	106	0.683	6	151	0.768	6.7	181	0.456	4.2
17	0.512	4	107	0.672	6	152	0.786	6.4	182	0.542	5
18	0.535	4.51	108	0.679	6	153	0.747	6	183	0.552	4.8
19	0.524	4	109	0.708	6	154	0.785	7	184	0.560	5
20	0.534	4	110	0.709	6.037	155	0.849	7	185	0.532	4.8
21	0.498	4.1	111	0.705	6	156	0.757	7	186	0.546	5
22	0.523	4	112	0.676	6	157	0.812	7.66	187	0.543	4.7
23	0.521	4	113	0.710	6	158	0.845	7	188	0.575	5
24	0.519	4	114	0.677	5.81	159	0.799	6.8	189	0.529	4.5
25	0.519	4	115	0.679	6	160	0.678	6	190	0.518	4.5
26	0.537	4	116	0.713	6	161	0.735	6.5	191	0.540	4.8
27	0.541	4.7	117	0.649	5.55	162	0.763	6.5	192	0.517	4.5
28	0.557	4.77	118	0.696	6	163	0.720	6	193	0.534	4.7
29	0.519	4	119	0.705	6	164	0.727	6.5	194	0.580	5
30	0.502	4	120	0.680	5.77	165	0.772	7	195	0.509	4

### 3. RESULTS AND DISCUSSION

For each studied plate were measured the amplitudes of two successive pulses and then applying equation (4), was determined the attenuation coefficient  $\alpha$ . For each type of material were made five measurements, making then statistical processing. The results and final values obtained are presented in Table 3.

Table 3. Experimental results

Code of samples	Thickness d [mm]	Amplitudes				$\alpha_1$ [dB/mm]	$\alpha_2$ [dB/mm]	$\alpha_3$ [dB/mm]	$\alpha$ average [dB/mm]
		A0	A1	A2	A3				
110	6.037	682	594	552	512	0.198767	0.105507	0.10823	0.137501
114	5.81	488	362	180	100	0.44651	1.04453	0.878735	0.789925
120	5.77	678	398	300	120	0.801895	0.425518	1.379341	0.868918
117	5.55	470	380	206	142	0.332664	0.958257	0.582266	0.624396

Code of samples	Thickness d [mm]	Amplitudes				$\alpha_1$ [dB/mm]	$\alpha_2$ [dB/mm]	$\alpha_3$ [dB/mm]	$\alpha$ average [dB/mm]
		A0	A1	A2	A3				
157	6.71	1174	910	660	464	0.329737	0.41579	0.456113	0.400547
158	7.05	842	806	352	270	0.053836	1.020688	0.326749	0.467091
159	6.56	1266	666	446	342	0.850486	0.530913	0.351551	0.57765
164	6.01	934	858	638	368	0.122661	0.428175	0.795251	0.448696
28	4.77	702	342	290	282	1.30948	0.300327	0.050939	0.553582
27	4.7	544	438	350	242	0.400531	0.414494	0.681926	0.498984
21	4.1	626	402	372	296	0.938284	0.164308	0.484152	0.528915
18	4.51	1070	360	282	210	2.097921	0.470303	0.56776	1.045328
185	4.42	1010	812	410	342	0.428802	1.342861	0.35637	0.709344
187	4.6	1292	724	620	338	1.093582	0.292813	1.145543	0.843979
190	4.17	962	640	468	376	0.848897	0.651962	0.455914	0.652258
191	3.95	820	724	444	418	0.273799	1.075218	0.132692	0.493903

In Figure 3 are compared the attenuation coefficient for tested plates. Within the same types of material were obtained different results - with quite large variations of the attenuation coefficient, which indicates the anisotropic nature of the plates, even in the same conditions of manufacturing technology.

The most homogeneous plates in terms of attenuation coefficient values were recorded for composites type 3 and 4 (with 6 stratimat layers of 300 g/m<sup>2</sup> and 4 layers of fiberglass, obtained by low pressure respectively high pressure).

Composites type 4 (obtained by high pressure) has a good behavior, being characterized by the higher attenuation coefficient. For the other types of composites 1 and 2, the values of attenuation coefficient indicate lower values as shown in Figure 3, but the differences between composites are not essential.

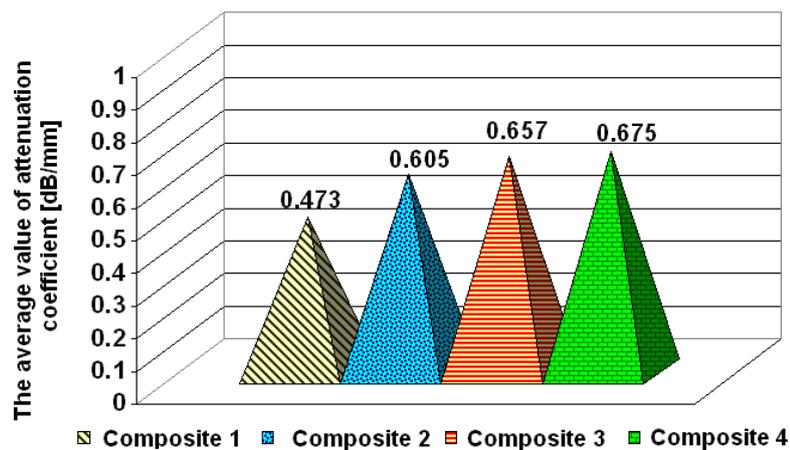
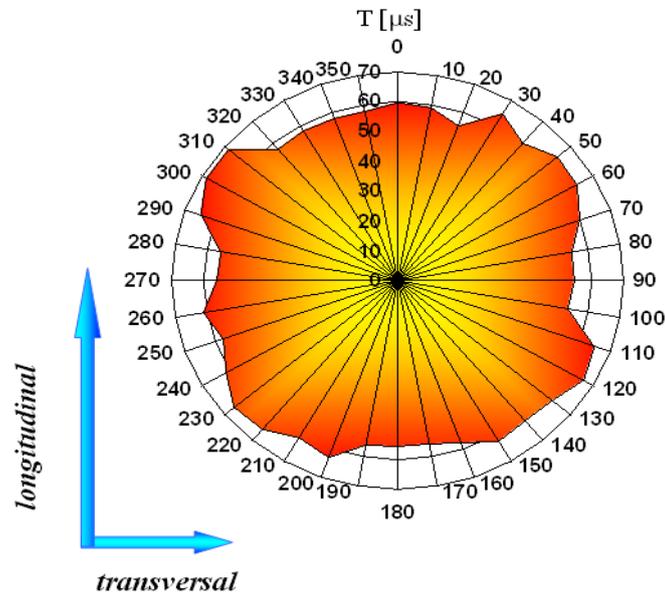


Fig.3. The variation of attenuation coefficient for each type of tested composite



**Fig.4.** The variation of ultrasound time propagation

It is known that the anisotropic structure of the composite influence both the non-mechanical and mechanical properties. For this reason, an anisotropy test was done with ultrasound method too. It was measured the time of ultrasound propagation in different points fixed by polar coordinates (see Figure 2). Successive measurements were recorded in the five points on the plate, after which they were processed statistically and presented in the graph in Figure 4. Time wave propagation is expressed in microseconds.

## 5. CONCLUSIONS

The results of this study revealed that the composite structure, the thickness of plates and the manufacturing process directly influences the values of acoustic attenuation coefficient in terms of good properties of ultrasound attenuation. Also, the used method explores the anisotropy of plates without deterioration of structure.

## 6. ACKNOWLEDGEMENTS

This paper is supported by the Sectoral Operational Programme Human Resources Development (SOP HRD), financed from the European Social Fund and by the Romanian Government under the contract number POSDRU POSTDOC-DD, ID59323.

## REFERENCE

- [1]. **Bucur, V.:** *Acoustic of wood*. Springer-Verlag Berlin Heidelberg New York, 2006
- [2]. **Cerbu, C., Curtu, I., Ciofoaia, V., Rosca I. C., Hanganu, L. C.,** *Effects of the Wood Species on the Mechanical Characteristics in Case of Some E-Glass Fibres/Wood Flour/Polyester Composite Materials*, in Rev. Materiale Plastice, MPLAAM 47 (1) 2010, Vol. 47, nr. 1 –martie 2010, Bucuresti Romania, pp.109-114, 2010.
- [3]. **Cosoreanu, C., Curtu, I., Lunguleasa, A., Lica D., Porojan M., Brenci, L., Cismaru, I., Iacob, I.,** *Influence of Synthetic and Natural Fibers on the Characteristics of Wood-Textile Composites*, Revista Materiale Plastice vol. 46, nr. 3 Sept. 2009, Bucuresti, p. 305-309, 2009.
- [4]. **Curtu Ioan, Stanciu Mariana Domnica, Ciofoaia Vasile:** *The modal analysis of plates made of woven composite materials*, în Buletinul AGIR, ISSN 1224-7928, An XVI, nr. 1/2011,
- [5]. **Grimberg, R., Curtu, I., Savin, A., Stanciu, M. D., Andreescu A., Leitoiu S., Bruma A., Barsanescu P,** *Elastic Waves Propagation in Multilayered Anisotropic Composite – Application to Multilayered Lignocellulose Composite*, in Proc. of The 7<sup>th</sup> Edition of International Conference „Wood Science and Engineering in the Third Millennium”, ICWSE 2009, Brasov, pp. 688-695, 2009.
- [6]. **Grimberg R, Savin A., Curtu I., Stanciu M. D, Lica D., Cosoreanu C,** *Assesment of wood using air-coupled US transducer*, in Proceedings of 17th WOOD NDT International Nondistructive testing and Evaluation of Wood Symposium – Vol II, 14-16 September 2011, Sopron Ungaria, ISBN 978-963-9883-83-3, p. 427 – 434
- [7]. **Stanciu M. D., Curtu I.,** *Using Advanced Method To Determine The Acoustical Parameter Of Lignocellulose Composite Materials*, in Proceedings of the 12<sup>th</sup> International Conference AFASES 2010, organizata de Academia Fortelor Aeriene Henri Coanda din Brasov, 27-29 mai 2010.
- [8]. **Terciu O. M., Curtu I, Cerbu C., Stanciu M.D.,** *Structures of composite materials reinforced with natural fibres subjected to mechanical stresses* , in Proceedings of The 4th International Conference on Structural Analisys of Advanced Materials – ICSAAM 2011, ISSN 2247-8337, Sinaia 7-11 septembrie 2011, pe CD, pp.339 – 346.
- [9]. **Tran Ich Thinh, Tran Huu Quoc,** *Finite element modeling and experimental study on bending and vibration of laminated stiffened glass fiber/polyester composite plates*, Computational Materials Science, 2010.
- [10]. \*\*\* Lucrari de laborator INCDFT –NDT Iasi, Grimberg R